



# *Communication* **High-Efficiency Achromatic Metalens Topologically Optimized in the Visible**

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**Abstract:** Metalens, composed of arrays of nano-posts, is an ultrathin planar optical element used for constructing compact optical systems which can achieve high-performance optical imaging by wavefront modulating. However, the existing achromatic metalenses for circular polarization possess the problem of low focal efficiency, which is caused by the low polarization conversion efficiencies of the nano-posts. This problem hinders the practical application of the metalens. Topology optimization is an optimization-based design method that can effectively extend the degree of design freedom, allowing the phases and polarization conversion efficiencies of the nano-posts to be taken into account simultaneously in the optimization procedures. Therefore, it is used to find geometrical configurations of the nano-posts with suitable phase dispersions and maximized polarization conversion efficiencies. An achromatic metalens has a diameter of 40  $\mu$ m. The average focal efficiency of this metalens is 53% in the spectrum of 531 nm to 780 nm by simulation, which is higher than the previously reported achromatic metalenses with average efficiencies of 20~36%. The result shows that the introduced method can effectively improve the focal efficiency of the broadband achromatic metalens.

**Keywords:** achromatic metalens; topology optimization; focal efficiency; polarization conversion efficiency



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## **1. Introduction**

As a planar optical element developed from metamaterials, the metalens can realize flexible modulation of light in the subwavelength scale, which has promising prospects in building lightweight and compacting optical systems when compared to conventional lenses [\[1\]](#page-8-0). It can be used in many applications [\[2\]](#page-8-1) such as beam generators [\[3,](#page-8-2)[4\]](#page-8-3), optical holographic imaging  $[5,6]$  $[5,6]$ , and virtual shaping  $[7,8]$  $[7,8]$ . However, the metalens has a dispersion problem which is inherent to the diffractive element [\[9\]](#page-8-8).

To solve this problem, the parameter optimization method has been used to design achromatic metalens. This method is used to change the values of the geometric parameters of the nano-posts, in order to establish a library, and then to assemble the achromatic metalens based on the phase matching principle. An achromatic metalens [\[10\]](#page-8-9) was designed based on the propagation phase modulation and work at three independent wavelengths of 1300 nm, 1550 nm, and 1800 nm, with the corresponding focal efficiencies of 15%, 10%, and 21%, respectively. Different nano-posts, including square nano-posts [\[11](#page-8-10)[,12\]](#page-8-11), circular nanoposts [\[13](#page-8-12)[,14\]](#page-8-13), hollow circular nano-posts [\[15\]](#page-8-14), and nano-posts with a mixture of shapes [\[16\]](#page-8-15), were likewise used to design polarization-independent metalenses in the continuous spectrum. The combination modulation  $[17–24]$  $[17–24]$  of the geometric phase and propagation phase was used to design achromatic metalenses by using rectangular nano-posts, with advantages in processing technology. However, the focal efficiencies of these metalenses did not exceed 40%. The low focal efficiencies are due to the orthogonal transformation of circular polarization states and the low polarization conversion efficiencies of the nano-posts. The polarization conversion efficiency is defined as the ratio of the field intensity of orthogonal light in the scattered field to the incident field. These are caused by the insufficiency of

the design freedom of the nano-posts, such as the geometric parameters of the rectangular Inc design freedom of the nano-posts, such as the geometric parameters of the rectangular<br>nano-posts. The insufficiency problem of the design freedom hinders the maintenance of maximum polarization conversion efficiency of the nano-post, while satisfying the required<br>maximum polarization in the current design mathede of schramatic metaleness. phase dispersion in the current design methods of achromatic metalenses. to the objective function and constraints. It is equivalent to extending the design freedom,

Topology optimization originated from Michell's [25] truss design research in 1904. It has been applied in electromagnetic waves, including beam splitters [\[26](#page-9-2)[,27\]](#page-9-3), photonic n has been applied in electromagnetic waves, including beam spillters [26,27], photonic<br>crystals [\[28,](#page-9-4)[29\]](#page-9-5), and metamaterials [\[30–](#page-9-6)[33\]](#page-9-7). Topology optimization has been used in the global optimization of the metalens to improve its performance, for example the highefficiency achromatic metalens [\[34\]](#page-9-8), but is rarely used in the nanopillar optimization of the emetalens. Different from the parameter optimization method, topology optimization is metalens. used to find the optimal distribution of materials in a given design domain according to the ased to find the optimal distribution of materials in a given design domain according to the<br>objective function and constraints. It is equivalent to extending the design freedom, which is beneficial to find the optimized nano-post with suitable phase dispersion and maximum<br>polarization conversion efficiency. Therefore, we use the topology ontimization to ontimize polarization conversion efficiency. Therefore, we use the topology optimization to optimize the nano-posts and assemble the high-efficiency achromatic metalens based on the library composed of the obtained nano-posts.

#### **2. Materials and Methods**

An achromatic metalens can convert the incident plane wave of any wavelength An achromatic metalens can convert the incident plane wave of any wavelength<br>in the working spectrum into the convergent spherical wave and make it focus on the<br>came focal gost (Figure 1). Therefore the phase profile on th in the working spectrum into the convergent spherical wave and make it focus on the same focal spot (Figure [1\)](#page-1-0). Therefore, the phase profile on the metalens must satisfy the following condition [\[35\]](#page-9-9):

$$
\varphi(r,\lambda) = -\frac{2\pi}{\lambda} \left( \sqrt{r^2 + f^2} - f \right) + C(\lambda). \tag{1}
$$

where  $\lambda$  is the wavelength of the incident wave, *r* is the radial coordinate on the metalens,<br>and f is the focal longth:  $C(\lambda)$  is an additional phase shift as a spectral dorror of freedom. and *f* is the focal length;  $C(\lambda)$  is an additional phase shift as a spectral degree of freedom, which is linear to the reciprocal of the wavelength  $\lambda$ . The phase profile can be satisfied by controlling the arrangement of  $TiO<sub>2</sub>$  nano-posts (Figure [2a](#page-2-0)).

<span id="page-1-0"></span>

**Figure 1.** Sketch for the cross-section of an achromatic metalens. **Figure 1.** Sketch for the cross-section of an achromatic metalens.

<span id="page-2-0"></span>

**Figure 2. (a)** The structure unit diagram of the achromatic metalens, where the gray rectangular block is the TiO<sub>2</sub> nano-post; (**b**) sketch for the computational domain  $Ω$ . The upper and lower domains  $Ω<sub>p</sub>$ are the perfectly matched layers (PMLs), which are used to suppress the boundary reflection. The substrate domain is  $\Omega_s$ , and the grey section is the design domain  $\Omega_d$ .

There are two approaches for the phase modulation of the achromatic metalens. The There are two approaches for the phase modulation of the achromatic metalens. The first is the propagation phase modulation. It is favorable to design high-efficiency first is the propagation phase modulation. It is favorable to design high-efficiency metalens with the absence of orthogonal polarization conversion. However, the dual constraints of phase and phase dispersion severely elongate the nano-posts, which poses a problem for processing technology. The second approach is the combination modulation of the geometric phase and propagation phase, which reduces the processing challenges due to phase dispersion as the only physical quantity required to be considered in the optimization process of the nano-post. However, the achromatic metalens possess the problem of low focal efficiency. In consideration of processing technology, the second approach was adopted in our work so that the focal efficiency of orthogonal circularly polarized light could be enhanced to the greatest extent. Thus, in the working spectrum, Equation (1) can be split into two parts for the second approach [\[23\]](#page-9-10):

$$
\varphi(r,\lambda) = \varphi(r,\lambda_d) + \Delta\varphi(r,\lambda). \tag{2}
$$

where  $\lambda_d$  is the design wavelength. The first term  $\varphi(r,\lambda_d)$  on the right side of Equation (2) is the target phase profile at the design wavelength  $\lambda_d$ , independent of the wavelength  $\lambda$ . It can be satisfied by rotating the nano-posts based on the geometric phase principle. For the left-handed circularly polarized incident light  $[1, i]^T$ , the transmitted electric field can be be described by the Jones vector: described by the Jones vector:

$$
E_t = \frac{t_u + t_v}{2} \begin{bmatrix} 1 \\ i \end{bmatrix} + \frac{t_u - t_v}{2} \exp(i \cdot 2\theta) \begin{bmatrix} 1 \\ -i \end{bmatrix}.
$$
 (3)

where  $t_u$  and  $t_v$  represent complex transmission coefficients, with the incident light polarized along the long and short axes of the cross section of the nano-post, respectively; and  $\theta$  is the rotation angle of the nano-post. In addition to the origin left-handed circularly polarized light with a complex amplitude of  $(t_u + t_v)/2$ , the scattered field also carries cross-polarized light with complex amplitude of  $(t_u + t_v)/2 \exp(i \cdot 2\theta)$ , where  $2\theta$  is a wavelength-independent geometric phase related to the rotation angle *θ* of the nano-post. The second term  $\Delta \varphi(r,\lambda)$  in Equation (2) represents the phase difference between arbitrary and design wavelength: wavelength and design wavelength:

$$
\Delta \varphi(r,\lambda) = -2\pi \left(\frac{1}{\lambda} - \frac{1}{\lambda_d}\right) \left(\sqrt{r^2 + f^2} - f\right). \tag{4}
$$

$$
\frac{d\Delta\varphi}{d(2\pi c/\lambda)} = -\frac{1}{c}\bigg(\sqrt{r^2 + f^2} - f\bigg). \tag{5}
$$

The first equation in Equation (4) shows that  $\Delta \varphi(r,\lambda)$  is a linear function of the reciprocal wavelength  $1/\lambda$ . The second equation is the group delay, which is independent of the wavelength *λ* but dependent on the radial coordinate *r* on the metalens. Since the additional geometric phase is independent of the wavelength and does not interfere with the propagation phase, the group delay matching can only be achieved by adjusting the broadband propagation phase, which is related to the structure of the nano-post. Then, the optimization of the nano-post for the specific group delay is required.

#### **3. Topology Optimization of Nano-Post**

Topology optimization is used to mesh the design area, to determine whether the material in the grid cell should be retained or removed by numerical analysis. The material in every grid cell can be regarded as a degree of design freedom, increasing the design freedom of the nano-post. Thus, topology optimization can be used to optimize the structure of the nano-post, aiming for the most suitable phase and maximum polarization conversion efficiency. If group delay is the goal of the optimization model, the objective function can be written as  $\varphi(\lambda_1) - \varphi(\lambda_2)$ . However, this objective function is ill-posed. An additional undetermined basic phase  $\varphi_0$  at design wavelength  $\lambda_d$  is then introduced to control  $\varphi(\lambda_1)$ and  $\varphi(\lambda_2)$  to solve this problem. Therefore, the deviations between the current phase and the target phase at the preset wavelengths are used to define the objective function instead of the group delay. In consideration of the problem that the phase reset characteristic will cause an inaccurate interpolation calculation, the sum of the least square deviations of complex amplitudes at multiple wavelengths is selected as the objective function:

$$
\min F = \sum_{m} \left| \mathbf{E}_{srm} - \alpha_m e^{i\varphi_{tm}} \right|^2, \text{ in } \Omega_d; \text{s.t. } \nabla \times \left[ \mu_r^{-1} \nabla \times (\mathbf{E}_{sm} + \mathbf{E}_{im}) \right] - k_0^2 \varepsilon_r (\mathbf{E}_{sm} + \mathbf{E}_{im}) = 0, \text{ in } \Omega; \nabla \cdot \mathbf{E}_{sm} = 0, \text{ in } \Omega.
$$
\n(6)

where  $k_0 = 2\pi/\lambda$  is the free space wave number;  $\varepsilon_r$  and  $\mu_r$  are the relative permittivity and relative permeability of the nano-post, respectively; **E***sm* and **E***im* are the scattered and background field at *m*-th wavelength, respectively; *m* = 1, 2, 3 . . . represents the case for the *m*-th wavelength; **E***srm* is the electric field of the cross-polarized light; *α<sup>m</sup>*  $\exp(i \cdot \varphi_{tm})$  is the target electric field of the cross-polarized light;  $\alpha_m$  and  $\varphi_{tm}$  represent the amplitude and target phase, respectively. The amplitude *α<sup>m</sup>* is introduced as a parameter to be scanned to reduce the objective function value. Specifically, it is scanned downward from 0.9 to find the maximum amplitude value that can make the objective function value approach zero. The target phase *ϕtm* is calculated according to the target group delay and the basic phase *ϕ*<sup>0</sup> at the design wavelength, which can take any value and be realized by the subsequent structural rotations. Thus, the basic phase  $\varphi_0$  needs to be scanned as an additional parameter to make the optimized group delay closer to the target group delay value.

The density method of topology optimization [\[36\]](#page-9-11) is used to optimize the nano-post, where the density of dielectric material is treated as the design variable. To ensure robust evolution, the design variable is sequentially filtered and projected to derive the material density representing the geometrical configuration of the nano-posts. The filtered design variable is calculated using the PDE filter [\[37\]](#page-9-12). The filtered design variable can have an intermediate value, resulting in gray structure boundaries. To solve this problem, the filtered design variable is projected  $[38,39]$  $[38,39]$ . On the material interpolation, linear interpolation formula is used for air and dielectric materials  $TiO<sub>2</sub>$ :

$$
\varepsilon_r(\gamma_p) = \varepsilon_{ra} + \gamma_p(\varepsilon_{rm} - \varepsilon_{ra}), \text{ in } \Omega_d. \tag{7}
$$

where  $\varepsilon_{ra}$  and  $\varepsilon_{rm}$  are the relative permittivities of air and dielectric materials TiO<sub>2</sub>, respectively;  $\gamma_p$  is the material density.

In this optimization model, the governing equation is firstly solved with the current *fa* and then the design variable is evolved according to the adjoint sensitivity, which is the first order variational of the objective function to the design variable: which is the first order variational of the objective function to the design variable: *d* Ω

$$
\delta \hat{J} = \int_{\Omega_d} -\gamma_{fa} \delta \gamma d\Omega_d.
$$
 (8)

where *γfa* is the adjoint variable of the filtered design variable. The topology optimization procedure is shown in [th](#page-4-0)e flowchart in Figure 3, where the finite element method is used to solve the wave equation and the design variable is evolved using the method of moving asymptotes. For more details of topology optimization refer to Supplementary Material. asymptotes. For more details of topology optimization refer to Supplementary Material. procedure is shown in the flowchart in Figure 3, where the finite element method is used

<span id="page-4-0"></span>

**Figure 3.** Flowchart for the topology optimization procedure. **Figure 3.** Flowchart for the topology optimization procedure.

#### **4. Results and Discussion**

**4. Results and Discussion**  formly sampled in the range of 0–2π and substituted into the topology optimization model or the nano-posts (rigure *za*). Taking the nano-post with the target group delay or 7 is<br>as an example, the simulated group delay and polarization conversion efficiency of the topologic[a](#page-5-0)lly optimized nano-post are obtained (Figure 4a). When the basic phase  $\varphi_0$ Twenty values of the basic phase *ϕ*<sup>0</sup> at the designed wavelength of 600 nm are uniof the nano-posts (Figure [2a](#page-2-0)). Taking the nano-post with the target group delay of 7 fs

is 0.3 $\pi$ , the group delay of the optimized nano-post 6.98 fs is closer to the target group delay, and the polarization conversion efficiency of the optimized nano-post is 88% at the designed wavelength. Figure [4b](#page-5-0) shows the phase of the optimized nano-post with the<br>hasis phase  $\alpha$ , of 0.2 $\pi$  is linear to the fracus ay in the apartum from 521 nm to 780 nm basic phase  $\varphi_0$  of 0.3 $\pi$  is linear to the frequency in the spectrum from 531 nm to 780 nm, and the broadband polarization conversion efficiency is no less than 40%. Therefore, this optimized nano-post can be extracted and placed at the position where the required group delay is 7 fs.

<span id="page-5-0"></span>

of the topology optimized nano-post under different basic phases  $\varphi_0$  at the design wavelength; (b) the phase (blue line) and polarization conversion efficiency (red line) of the structure unit (vertical view) composed of SiO<sub>2</sub> substrate (blue area) and TiO<sub>2</sub> nano-post (gray area) obtained by topology<br> $\frac{1}{2}$ composition with a sacre prime of SiON II and Specially health (cf. time to you have **Figure 4.** (**a**) The group delay (blue line) and polarization conversion efficiency (PCE) (red line) optimization with a basic phase of  $0.3\pi$  in the spectrum from 531 nm to 780 nm.

Different values of group delay are put into the topology optimization model of the<br>none a sected with a subsidered are put into the topology optimization model of the Based on this established library, an achromatic metalens is designed with a diameter of  $\frac{1}{2}$ Form and the over according to the discrete distribution of the group design wavelength, and the discrete phase realized by the nano-posts is consistent with the ideal phase profile (Figure 6). Figure 7a shows the focal s[po](#page-7-0)ts on the designed focal<br>langular f.179.50 was at account disportaneouslap the in the gauge of 521 and to 790 and The maximum and minimum focal lengths of these wavelengths are 187.07  $\mu$ m and 164.37  $\mu$ m, respectively. The differences from the designed focal length are within 14.12  $\mu$ m with the relative arror of 7.91%. The focal officionar is the ratio of the Boynting vector integral of the cross-polarized light within three times FWHM to the Poynting vector integral of the transmitted light. Through the above definition, the focal efficiencies of the achromatic<br>moteless are calculated at nine wavelengths in the working spectrum (Figure 7d). The maximum and minimum focal efficiencies are 58% and 44%, respectively. In the whole working spectrum, the average efficiency is approximately 53%, higher than the previously<br>reported achromatic metalens with average efficiencies of 20~36% [19.40]. When compared with other achromatic metalenses, the high focal efficiency of the achromatic metalens is manny because of the riigh polarization conversion efficiency of the nano-posts. Further,<br>another achromatic metalens is also designed with a diameter of 20 μm and NA of 0.22. The maximum relative focal length error of the metalens is 7.97%, and the average efficiency for the spectrum from 551 him to 760 him is 56%, which are an close values when compared<br>with the performance of the achromatic metalens with NA of 0.11. nano-posts and the optimized nano-posts are entered into a library (some of them are shown in Figure [5\)](#page-6-0). For more details of nano-posts in the library refer to Supplementary Material. 40 µm and NA of 0.1 according to the desired distribution of the group delay and phase at length of 178.50 µm at several discrete wavelengths in the range of 531 nm to 780 nm. The relative error of 7.91%. The focal efficiency is the ratio of the Poynting vector integral of metalens are calculated at nine wavelengths in the working spectrum (Figure [7d](#page-7-0)). The reported achromatic metalens with average efficiencies of 20~36% [\[19](#page-8-17)[,40\]](#page-9-15). When compared mainly because of the high polarization conversion efficiency of the nano-posts. Further, the spectrum from 531 nm to 780 nm is 56%, which are all close values when compared

<span id="page-6-0"></span>

Figure 5.  $(a-f)$  The phase and polarization conversion efficiency (PCE) of some structure units (vertical view) composed of  $SiO<sub>2</sub>$  substrates (blue area) and  $TiO<sub>2</sub>$  nano-posts (gray area) in the library. tical view) composed of SiO2 substrates (blue area) and TiO2 nano-posts (gray area) in the library.

<span id="page-6-1"></span>

Figure 6. The actual discrete phase realized by the topologically optimized nano-posts (colored dot) and the ideal phase profile (black line) on the achromatic metalens, the bottom of which is the oblique view of the overall structure of the achromatic metalens along with the radius direction and top view of each local magnification.

<span id="page-7-0"></span>

Figure 7. (a) Normalized electric field near the focal plane in the spectrum from 531 nm to 780 nm; (b) normalized point spread function (PSF);  $(c-e)$  the focal lengths  $(c)$ , focal efficiencies (d), and FWHM (**e**) of the two metalenses with different NA values in the spectrum 531 nm~780 nm. FWHM (**e**) of the two metalenses with different NA values in the spectrum 531 nm~780 nm.

## **5. Conclusions 5. Conclusions**

When targeting the problem of low focal efficiency of achromatic metalenses, we used the topology optimization method to optimize the structures of  $TiO<sub>2</sub>$  nano-posts and derive the achromatic metalenses with an average focal efficiency of 53% in the spectrum from  $\frac{1}{100}$ 531 nm to 780 nm. A library of the TiO<sub>2</sub> nano-posts was derived by solving a topology<br>solving a topology permization model to achieve maximum broadband focal efficiency at each group delay value. Based on the library, we assembled an achromatic metalens with a diameter of 40 µm value. Based on the library, we assembled an achromatic metalens with a diameter of 10 function and NA of 0.11 by combining the geometric phase and the propagation phase modulation. The maximum focal efficiency of the achromatic metalens was 58%. Topology optimization The maximum focal efficiency of the achromatic metalens was 58%. Topology optimization greatly increased the design freedom of the  $TiO<sub>2</sub>$  nano-posts. It effectively solved the greatly increased the design freedom of the  $TiO<sub>2</sub>$  nano-posts. It effectively solved the problem that the group delay and the polarization conversion efficiency cannot be taken tively solved the problem that the group delay and the polarization conversion efficiency into account simultaneously due to insufficient design freedom in the previous parameter optimization method. This work can be of significance in the promotion of high lightweight  $\frac{1}{2}$  previous previous parameter of significance in the process can be of significance in the process can be of significance in the process can be obtained in the process can be obtained in the process can be obtaine and high integration of broadband in the micro-imaging system. optimization model to achieve maximum broadband focal efficiency at each group delay

[www.mdpi.com/article/10.3390/nano13050890/s1,](https://www.mdpi.com/article/10.3390/nano13050890/s1) Table S1: Group delay and average polarization conversion efficiency of the nano-post in the library. **Supplementary Materials:** The following supporting information can be downloaded at: [https://](https://www.mdpi.com/article/10.3390/nano13050890/s1) **Author Contributions:** Conceptualization, L.Z., C.W. and Y.D.; methodology, L.Z., C.W. and Y.D.; software, L.Z. and C.W.; validation, L.Z., Y.W. and C.W.; formal analysis, Y.L. and Y.H.; investigation, Y.L. and Y.H.; resources, Y.D.; data curation, L.Z.; writing—original draft preparation, L.Z.; project administration, Y.D.; funding acquisition, Y.D. All authors have read and agreed to the published version of the manuscript.

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