

Repairing surface defects of Zr-based metallic glass ribbons by nanosecond pulsed laser irradiation



Jingtao Wang^a, Hongyang Zhang^a, Zhiyu Zhang^b, Jing Hong^a, Yongfeng Qian^a, Hu Huang^{a,*}, Jiwang Yan^c

^a Key Laboratory of CNC Equipment Reliability, Ministry of Education, School of Mechanical and Aerospace Engineering, Jilin University, Changchun, Jilin 130022, China

^b Key Laboratory of Optical System Advanced Manufacturing Technology, Changchun Institute of Optics, Fine Mechanics and Physics, Chinese Academy of Sciences, Changchun, China

^c Department of Mechanical Engineering, Faculty of Science and Technology, Keio University, Yokohama 223-8522, Japan

ARTICLE INFO

Article history:

Received 5 September 2022

Received in revised form 15 November 2022

Accepted 25 November 2022

Available online 20 December 2022

Keywords:

Amorphous materials

Laser processing

Metallic glass ribbon

Surface defects

Nanosecond pulsed laser

ABSTRACT

The metallic glass ribbons (MGRs) industrially produced by the single roller melt-spun method have many surface defects such as pits and scratches. In this study, it was attempted to repair the surface defects of Zr-based MGRs via nanosecond pulsed laser irradiation. The experimental results showed that the roughness of laser-repaired surfaces was significantly reduced compared to the melt-spun surface, and the surface topographies and morphologies were sensitive to the laser parameters. With optimal laser parameters, the smooth and defect-free surface could be achieved. This work offers a convenient and high-efficiency approach for repairing the surface defects of MGRs.

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1. Introduction

With some unique characteristics such as high strength, high corrosion resistance, and excellent wear resistance [1,2], metallic glass ribbons (MGRs) are very promising structural and functional materials. For MGRs, previous studies mainly focused on solving their size [3,4] and surface oxidation problems [5], and the surface quality issues are generally ignored. Specifically, the MGRs surfaces suffer from various defects, such as pits and scratches which severely limit their engineering applications. The conventional methods such as chemical mechanical polishing [6] and electrochemical polishing [7], may be not applicable for repairing the surface defects due to the flexibility and thin structure of MGRs. While, laser processing on the other hand has been widely used to fabricate micro/nano structures on bulk metallic glasses [8–11], as well as modify their surface mechanical properties [12–15]. For example, Qian et al. [9] used a nanosecond pulsed laser to fabricate micro-convex array structures on a Zr-based MG surface which tuned the light reflection characteristic. By laser nitriding, surface hardness of the Zr-based MG was significantly increased by Hong et al. [12]. With features of non-contact processing and high heating/cooling rates, nanosecond pulsed laser irradiation was attempted here to repair the surface defects of

MGRs and improve their surface quality. By optimizing the irradiation parameters, defect-free smooth surfaces were successfully achieved. The roughness and three-dimensional topographies of the laser-repaired surfaces were characterized, and the surface morphology evolution was analyzed. This work offers a convenient and high-efficiency approach for repairing the surface defects of MGRs.

2. Materials and experiments

The Zr-based MGRs with nominal compositions of $Zr_{41.2}Ti_{13.8}Cu_{12.5}Ni_{10}Be_{22.5}$ were prepared by single roller melt-spinning under vacuum. All ribbons with a cross section of about $0.05 \text{ mm} \times 4 \text{ mm}$ were cut into slices with the length of 20 mm. Before laser processing, the amorphous feature of the ribbons was confirmed by X-ray diffraction (XRD, D8 Advance, Bruker, Germany). Then, the samples were placed in an atmosphere chamber with flowing argon, and the pressure was maintained at 0.01 MPa. A nanosecond pulsed laser (SP-050P-A-EP-Z-F-Y, SPI Lasers, UK) with a wavelength of 1064 nm was used for irradiation experiments. The laser beam diameter was about $43 \mu\text{m}$ with a Gaussian energy distribution. The pulse width and repetition frequency were 20 ns and 353 kHz, respectively. Generally, the peak laser power intensity (I), overlap rate (r), number of irradiation cycles (N) and scanning speed (v) would greatly affect the surface quality. Therefore, these four parameters were investigated by orthogonal experiments, and

* Corresponding author.

E-mail address: huanghu@jlu.edu.cn (H. Huang).

an optimal set of parameters was obtained, i.e., $I = 3.85 \times 10^9 \text{ W/m}^2$, $r = 88.4\%$, $N = 6$ and $v = 900 \text{ mm/s}$. For the purpose of investigating the influence of each parameter on laser repairing, 20 cases of experiments were designed according to the optimal parameters, as listed in Table 1. The other parameters were kept constant when one parameter was varied.

Table 1
Experimental parameters for laser repairing.

Case	$I (\times 10^9 \text{ W/m}^2)$	$r (\%)$	N	$v (\text{mm/s})$
1	3.51	88.4	6	900
2	3.66	88.4	6	900
3	3.85	88.4	6	900
4	3.96	88.4	6	900
5	3.99	88.4	6	900
6	3.85	30.2	6	900
7	3.85	53.5	6	900
8	3.85	76.7	6	900
9	3.85	88.4	6	900
10	3.85	93.4	6	900
11	3.85	88.4	4	900
12	3.85	88.4	5	900
13	3.85	88.4	6	900
14	3.85	88.4	7	900
15	3.85	88.4	8	900
16	3.85	88.4	6	700
17	3.85	88.4	6	800
18	3.85	88.4	6	900
19	3.85	88.4	6	1000
20	3.85	88.4	6	1100

After laser irradiation, the roughness and three-dimensional (3D) topographies of the irradiated areas were measured by the laser confocal scanning microscope (LCSM, OLS4100, Olympus, Japan). The measurement area was $256 \mu\text{m} \times 256 \mu\text{m}$, and the roughness values of five measurements were averaged. Furthermore, a tungsten filament scanning electron microscope (SEM, JSM-IT500A, JEOL, Japan) was used to characterize the morphology evolution of the laser-irradiated surfaces.

3. Results and discussion

Fig. 1(a)-(d) present the surface roughness (S_a) of the melt-spun surface and laser irradiated surfaces obtained under various I , r , N and v , respectively. As shown in Fig. 1(a), the melt-spun surface possesses a large S_a (namely, 419.6 nm), while the surface roughness of laser repaired surfaces decreases significantly. When the I increases, the S_a decreases first and then increases again, and the minimum S_a (namely, 61.8 nm) is obtained at $3.85 \times 10^9 \text{ W/m}^2$. In Fig. 1(b), the S_a decreases slowly and reaches a minimum value when the r is 88.4%. However, when further increasing the r to 93.4%, the change of S_a is very slight, demonstrating that the larger r has little significant effect on the surface roughness. Fig. 1(c) shows the change of S_a under different N , which is similar to the trend in Fig. 1(a). In addition, the S_a shows a negligible change when v increases from 700 to 1100 mm/s in Fig. 1(d), suggesting that the employed scanning speed has almost no effect on the roughness of the irradiated surfaces. From the above analysis, it is seen that the Zr-based MGRs can be repaired by nanosecond pulsed laser irradiation, and the best surface quality with S_a of

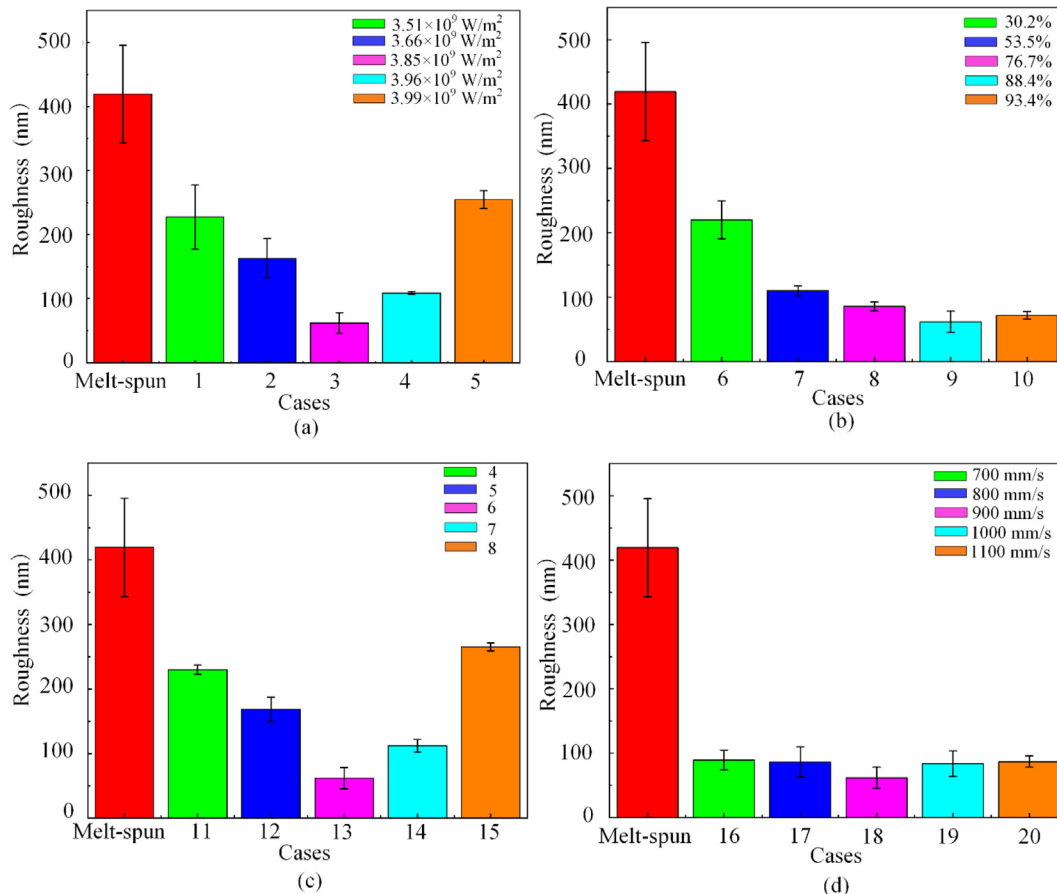


Fig. 1. S_a of the melt-spun and laser repaired surfaces obtained under various (a) peak laser power intensities, (b) overlap rates, (c) numbers of irradiation cycles, and (d) scanning speeds.

61.8 nm can be achieved under the optimal parameters according to the orthogonal design. In addition, it can be concluded that for the used parameter ranges, the peak laser power intensity, overlap rate and number of irradiation cycles have significant effects on the surface roughness, while the effect of the scanning speed is relatively slight.

To study the change in 3D topography, the melt-spun surface and representative laser-repaired surfaces are observed by using the LCSM, and the results are shown in Fig. 2. Fig. 2(a) and (b) indicate that after laser repairing, the peak-valley height of the surface decreases from 14 μm to 6 μm. Moreover, from Fig. 2(c), it is seen that the height of the repaired surface has less drastic fluctuation than that of the melt-spun. This can be attributed to the molten role of laser, and the molten material fills into the surface defects [16]. From Fig. 2(d), (b) and (g), it is noted that the peak-valley height of the repaired surfaces decreases first and then increases again when the I increases. Excessive molten material in the center of the pool flows to the edges when a relatively high I is applied [17,18], resulting in a larger surface height. As shown in Fig. 2(e), (b) and (h), the larger r leads to over melting, which in turn aggravates the re-solidification of the uneven surface [19]¹¹, making the surface height increase. Increasing the N prolongs the interaction time between the laser

and material and affects the degree of melting [20], but the redundant irradiation time would enhance the fluidity of the melt and cause an increase in surface height, as shown in Fig. 2(f), (b) and (i).

Fig. 3 presents the SEM morphologies of the Zr-based MGRs surfaces before and after laser repairing. For the melt-spun surface as shown in Fig. 3(a), the presence of many pits and scratches results in the high roughness and peak-valley height. Fig. 3(b) shows the SEM morphology of the laser repaired surface (case 3). No obvious pits and scratches can be observed, indicating that the defects on the original surface have been repaired. From Fig. 3(c) and (f), when the I is low, the surface defects are partly repaired due to inadequately melting of the material, and with the I increasing, the surface heat accumulates severely [17,21], causing the surface material to rapidly melt, evaporate and generate the ejection phenomenon, which eventually leads to an uneven ablated surface. In Fig. 3(d) and (g), it is evident that when the r increases, the surfaces become smooth gradually. As for Fig. 3(e) and (h), although the repetitive laser repairing greatly improves the surface quality, significant height difference appears on the repaired surfaces. This could be mainly due to the increasingly intense flow of the melt under surface tension and gravity, as well as the increasing depth of the molten layer [22,23].

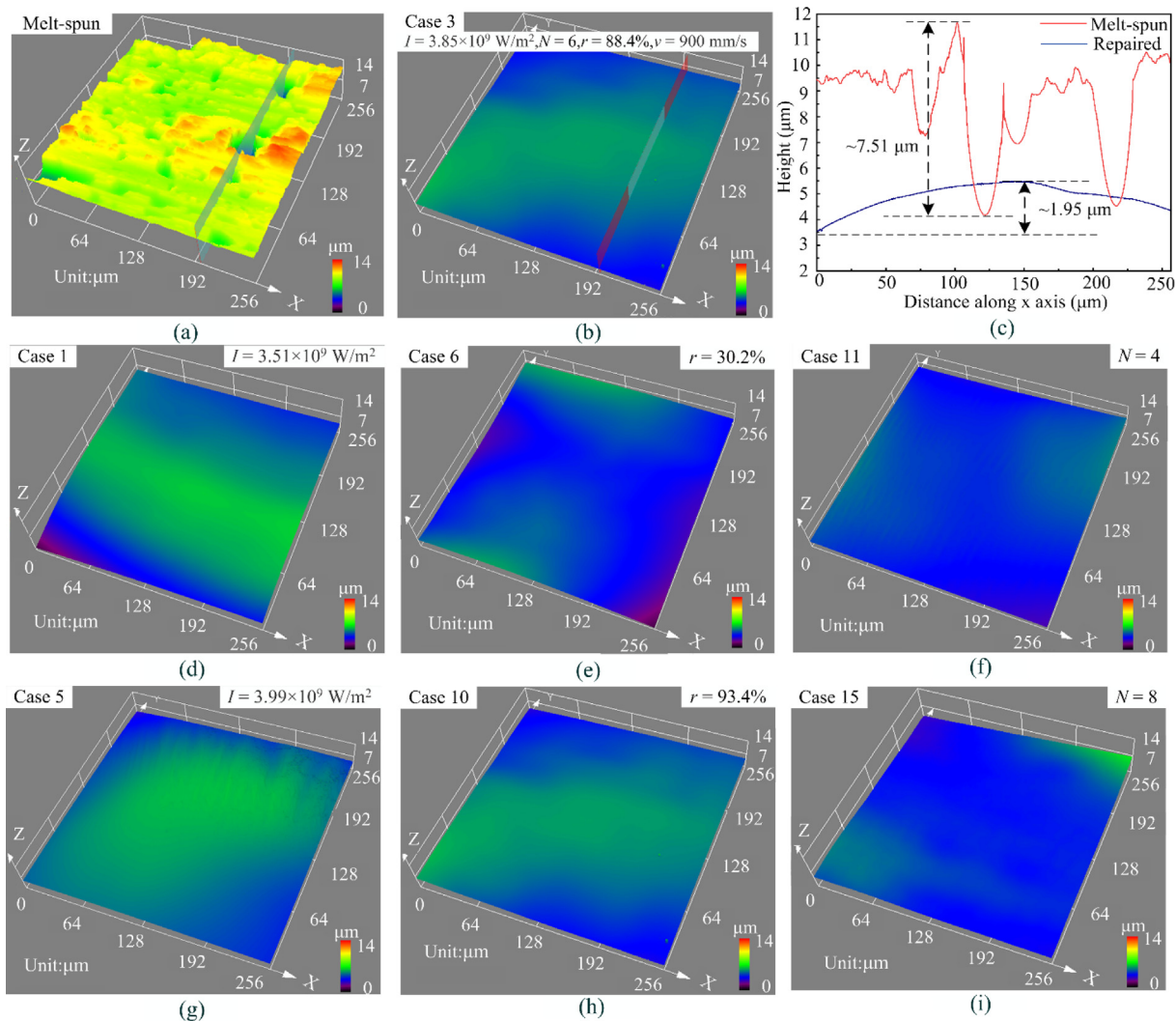


Fig. 2. 3D topographies of (a) melt-spun, (b) case 3, (d) case 1, (e) case 6, (f) case 11, (g) case 5, (h) case 10 and (i) case 15 surfaces. (c) shows the height of melt-spun and laser repaired surface (case 3).

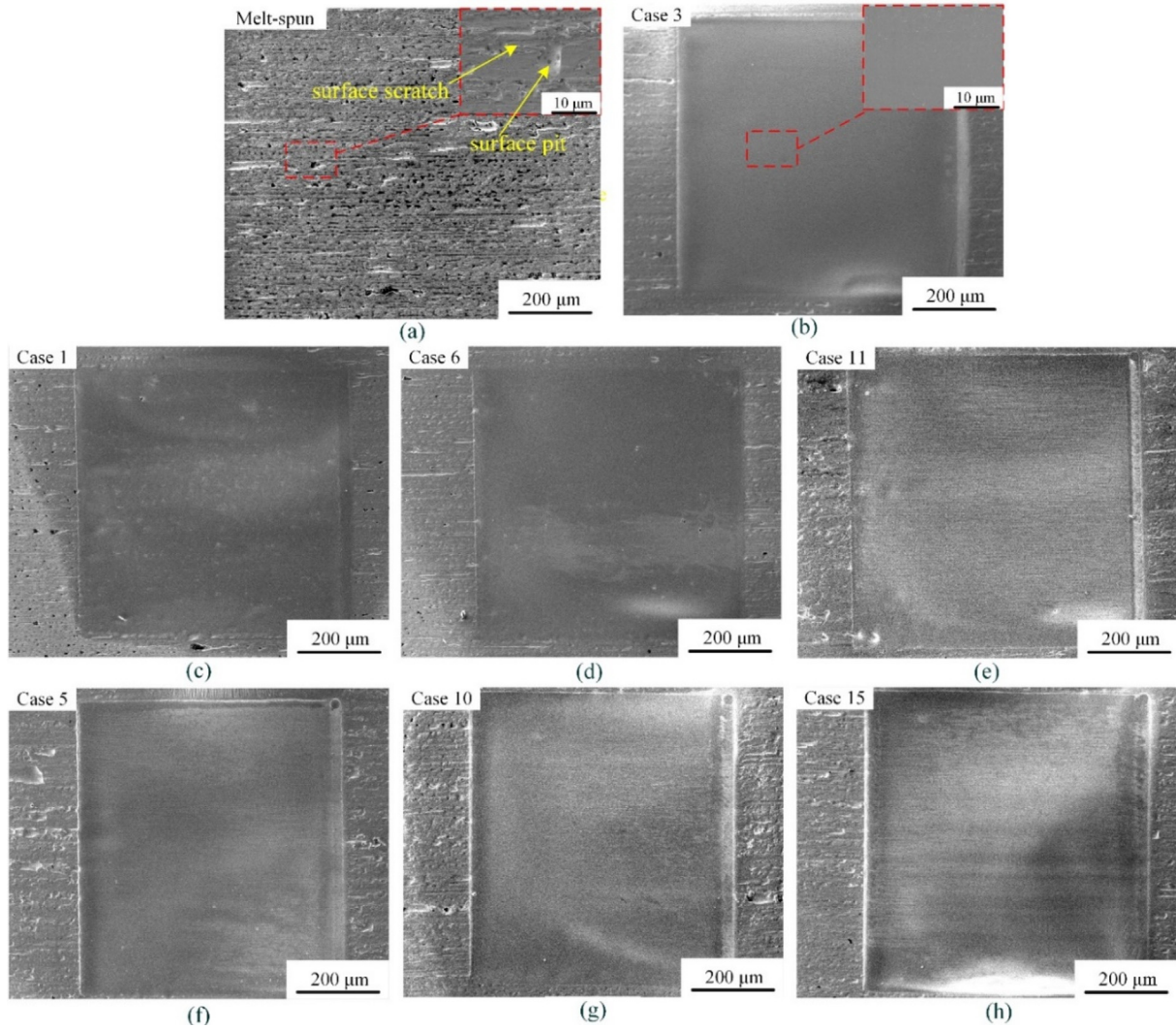


Fig. 3. SEM morphologies of (a) melt-spun, (b) case 3, (c) case 1, (d) case 6, (e) case 11, (f) case 5, (g) case 10, and (h) case 15 surfaces.

4. Conclusion

In summary, surface defects of Zr-based MGRs were successfully repaired via nanosecond laser irradiation in argon atmosphere. The influence of laser irradiation parameters on the 3D topographies and surface morphology evolution of the laser repaired areas was explored. Under optimal experimental conditions, the surface pits and scratches could be completely removed, and the surface roughness was decreased from 419.6 nm to 61.8 nm. The current finding offers a convenient and high-efficiency approach for repairing the surface defects of MGRs.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgements

This work was supported by the Natural Science Foundation of Jilin Province (20220101198JC) and the National Natural Science Foundation of China (Grant No. 51705197).

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