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The stacking fault annihilation in *a*-plane AlN during high-temperature annealing†

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Clarifying the defect evolution mechanism is the key to realizing high-quality non-polar AlN based materials and devices. In this work, the basal stacking fault density of the sputtered nonpolar *a*-plane wurtzite AlN (*a*-AlN) template decreased from 27100 cm⁻¹ to 5500 cm⁻¹ by high-temperature annealing and the underlying mechanism is systematically investigated by first-principle calculations. By analysing the minimum energy pathway during the elimination of the I₁-type stacking fault, it was found that two I₁-type stacking faults transform into one I₃-type stacking fault as the intermediate state and then annihilate. The highest energy barriers for eliminating and forming the I₁-type stacking default are 5.032 eV and 5.204 eV, respectively, explaining the phenomenon that the BSFD decreases at first and then increases with the increasing annealing temperature. In addition, the FWHMs of (11-20) XRC along different azimuth angles are nearly uniform instead of the normal ‘M’ shape, indicating that the crystal quality of *a*-AlN improved uniformly along different azimuth angles after high-temperature annealing. The results presented here are a significant step towards the synthesis of high-quality non-polar AlN material and non-polar light-emitting diodes.

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1. Introduction

AlN-based materials are promising for fabricating deep ultraviolet (DUV) photoelectric devices because of their wide and direct bandgaps. Currently, AlN-based DUV photoelectric devices are mainly fabricated on *c*-plane wurtzite AlN (*c*-AlN) because it is more mature to grow high-quality *c*-AlN on them than on other crystal planes.¹⁻³ However, there are strong spontaneous and piezoelectric polarization fields along the *c*-plane AlN, which can “tilt” the energy band and thus decrease the wavefunction overlap of the electron and hole carriers, which is named quantum-confined stark effect (QCSE).⁴ The QCSE decreases the internal quantum efficiency and thus hinders the development of AlN-based light-emitting diodes (LEDs).^{5,6} To date, several methods have been adopted to solve this problem, such as the growth of zincblende AlN (zb-AlN), the doping of quantum wells (QWs), and the

adoption of non-polar wurtzite AlN (wz-AlN).⁷⁻¹¹ Among these methods, growing thick zb-AlN is difficult since it is a metastable structure and the doping of QWs can just mitigate the QCSE instead of solving it. As a result, obtaining non-polar wz-AlN for the growth of non-polar LEDs is considered to be an effective method to eliminate polarization. For example, the *a*-plane wz-AlN (*a*-AlN) was grown on the *r*-plane sapphire (*r*-sapphire) substrate.

However, the growth of non-polar AlN is still challenging. There exists a large and inhomogeneous mismatch between the heterogeneous substrate and epitaxial layer. The mismatches between the *a*-AlN and *r*-sapphire substrate along the two perpendicular directions are 2.8% (tensile strain, parallel to the *c*-axis) and 13.1% (compressive strain, perpendicular to the *c*-axis), respectively.¹² Furthermore, the mosaics in *a*-AlN are more likely to rotate and tilt than those in *c*-AlN because the Al-N bond along the *a*-direction is weaker than that in the *c*-direction.¹³ Many efforts have been made to improve the crystalline quality of the hetero-epitaxial *a*-AlN layer.¹⁴⁻¹⁷ Miyagawa *et al.* optimized the epitaxial parameters and realized high-quality *a*-AlN on *r*-sapphire substrates with various off-angles.¹⁵ The high crystalline quality *a*-AlN was grown at 1250 °C on the 0.45°-off *r*-plane sapphire substrate. The full width at half maximum (FWHM) of X-ray diffraction rocking curves (XRC) of (11-20) plane *a*-AlN along *c/m*-direction are about 900/1250 arcsec. The high crystal quality *a*-AlN was grown by applying the epitaxial

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lateral overgrowth (ELO) method on patterned *a*-AlN templates.¹⁸ The FWHM of the ELO *a*-AlN along the *c*-plane reached 700 arcsec. However, the fabrication process of the patterned *a*-AlN substrate is complicated and the coalescence thickness of the *a*-AlN film is too thick (about 6 μm). Recently, high-temperature annealing (HTA) was adopted as an effective and simple method to improve the crystal quality of *c*-AlN and ultraviolet LEDs with high luminous efficiency have been demonstrated.^{19–22} Inspired by the results, Dinh *et al.* adopted high-temperature annealing (HTA) method to reduce the basal stacking fault density (BSFD) in non-polar *m*-plane *wz*-AlN, and the BSFD decreased from $\sim 1 \times 10^5$ to $\sim 5 \times 10^3 \text{ cm}^{-1}$.¹¹ Although the BSFD in the non-polar AlN by the HTA is not as low as expected, the HTA method has been shown to be a promising method. Therefore, the stacking faults annihilation mechanism during the HTA needs to be further understood.

In this work, the basal stacking fault (BSF) annihilation mechanism of in *a*-plane AlN during HTA was studied both experimentally and theoretically. The BSFD of the sputtered *a*-AlN template decreased from 27100 cm^{-1} to 5500 cm^{-1} by HTA. During the HTA process, the I_1 -type stacking faults move closer and further annihilate during the HTA process, and the I_3 -type stacking faults are formed in the intermediate state. This work will benefit the comprehension of the evolution mechanism of the basal stacking faults (BSFs) in *a*-AlN during HTA.

2. Experimental

A 200 nm *a*-AlN layer was deposited on a 2-inch (1–102) *r*-sapphire substrate using an ultra-high vacuum DC magnetron sputtering system. The whole process was under an ambient atmosphere of mixed nitrogen (N_2) and argon (Ar) at a pressure of 8×10^{-8} Torr, and the flow rates of N_2 and Ar were 120 sccm and 25 sccm, respectively. The sputtering power was 3500 W and the sputtering temperature was 600 °C. After the deposition, the *a*-AlN samples were annealed at 1500 °C, 1600 °C, 1650 °C, 1700 °C, and 1750 °C for 60 min in N_2 atmosphere. After that, the sputtered *a*-AlN templates were annealed at 1700 °C at different times (60–480 min).

XRD was used to characterize the crystal orientation and quality of the *a*-AlN templates. Transmission electron microscopy (TEM) was used to reveal the reduction of defects density. The climbing-image nudged elastic band (CI-NEB) method was employed to clarify the transition process of the stacking faults in *a*-AlN during HTA.²³ The Raman measurement was carried out to investigate the in-plane stress of the *a*-AlN templates.

3. Results and discussion

The large-scaled XRD 2θ - ω scan curves of the AlN templates under different annealing conditions are shown in Fig. S1 in ESI.† Based on Fig. S1,† it can be concluded that the AlN

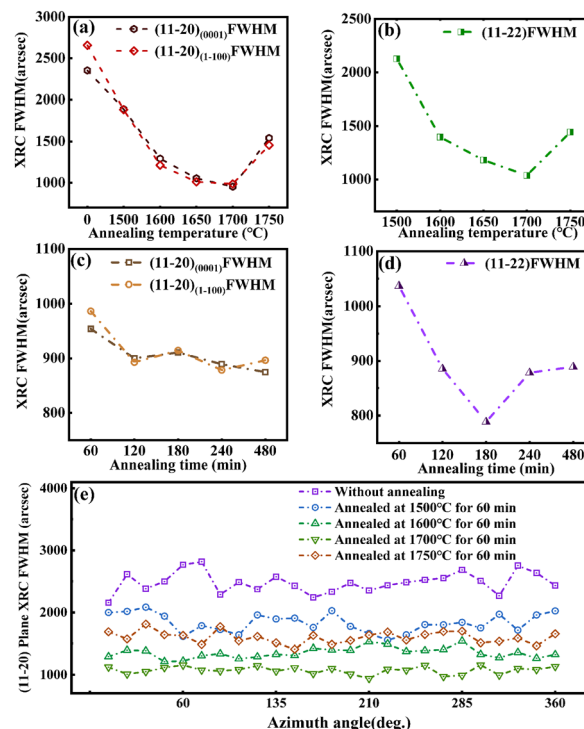


Fig. 1 (a) The FWHMs of (11-20)_[10-10] and (11-20)_[0001] plane XRC and (b) the FWHMs of (11-22) plane XRC for the *a*-AlN annealed at different temperatures for 60 min. (c) The FWHMs of (11-20)_[10-10] and (11-20)_[0001] plane XRC and (d) the FWHMs of (11-22) plane XRC for the *a*-AlN annealed at 1700 °C with different annealing times. (e) The FWHM of (11-20) XRC of *a*-AlN as a function of azimuth angles, for the *a*-AlN annealed at different temperature for 60 min.

templates are *a*-plane (11-20) preferred. Then, the XRC was taken to further characterize the crystal quality of the *a*-AlN templates. The FWHMs of the (11-20) plane XRC along the *c*/*m*-direction are shown in Fig. 1(a), which are widened by the partial dislocations (PDs) and the threading dislocations (TDs).^{24,25} As seen in Fig. 1(a), the FWHM decreases to the minimum at the annealing temperature of 1700 °C and then increases as the annealing temperature rises to 1750 °C. The FWHM of (11-20)_[0001]/(11-20)_[10-10] plane decreases from 2354/2656 arcsec (without annealing) to 954/986 arcsec (1700 °C annealing for 60 min), respectively. The crystal quality of the annealed *a*-AlN in this work is comparable to the optimal crystal quality of *a*-AlN fabricated on heterogeneous substrates.^{9,18} Furthermore, the FWHMs of (11-20) plane XRC along different azimuth angles are shown in Fig. 1(e), and the interval between each point is 15°. It is obvious that the FWHMs along different azimuth angles are approximately uniform instead of the normal ‘M’ shape, indicating that the crystal quality of *a*-AlN was improved evenly along different azimuth angles after HTA.¹⁴ As is well known, the FWHM of (11-22) plane XRC increases with the increase of BSFD.²⁴ The corresponding results are shown in Fig. 1(b) for the *a*-AlN under different annealing temperatures. From Fig. 1(b), we can obviously see that the FWHM of (11-22) plane XRC drops to the minimum (1036 arcsec) at the annealing temperature



of 1700 °C. The FWHM of (11-22) plane XRCs shows the same tendency as that of the (11-22) plane XRCs, which means that the PDs, TDs, and BSFD have the same trends with increasing annealing temperatures. It should be noted that the intensity of the (11-22) plane XRC for the *a*-AlN without annealing is too weak to be measured, and thus, there is no such data point in the curve of Fig. 1(b). The XRD phi-scan result is shown in Fig. S2 in the ESI.†

To investigate the effect of annealing time on the crystal quality of *a*-AlN annealed at 1700 °C, the FWHMs of (11-20)_[0001]/(11-20)_[10-10] and (11-22) plane XRC for the *a*-AlN annealed at 1700 °C with different annealing time are summarized in Fig. 1(c) and (d). Fig. 1(c) illustrates that the FWHMs of (11-20)_[0001]/(11-20)_[10-10] plane XRC are reduced slightly (no more than 10%) with the annealing time increasing from 60 min to 480 min. These results indicate that both the tilt and twist mosaics of the *a*-AlN layers are lightly influenced by the annealing time. Fig. 1(d) shows that the minimal FWHM of (11-22) plane XRC reaches 810 arcsec for the *a*-AlN annealed at 1700 °C for 180 min.

The modified Williamson–Hall model is an effective way to measure the lateral coherence length (LCL) of crystals, and thus the BSFD can be calculated. The Williamson–Hall-type peak width plots contain the (*h*₀-*h*₀) (*h* = 1, 2, 3) plane XRC scan reflections, but the FWHM of (30-30) plane XRC is not considered in the calculation (due to ref. 24). The LCL was estimated by fitting the FWHM of the XRC diffraction peak of (10-10) and (20-20). The equation for W–H analysis can be expressed as follows:

$$\Delta\omega_{\text{measure}} = \Delta\omega_{\text{mosaic}} + \frac{\lambda}{2L \sin(\theta_{hkl})} \quad (1)$$

where $\Delta\omega_{\text{measure}}$ is the FWHM of the (*hkl*) plane XRC, λ is the wavelength of the X-ray source ($\lambda = 0.15406$ nm), θ_{hkl} is the Bragg angle for the (*hkl*) reflection, $\Delta\omega_{\text{mosaic}}$ is the tilt angle for the mosaic. *L* represents the LCL and the BSFD of the AlN layer is calculated as 1/*L*. The fitting figures of the W–H analysis are shown in Fig. S3 in the ESI† and the results are

Table 1 The FWHMs of (*h*₀-*h*₀) plane XRC, LCL and calculated BSFDs of *a*-AlN templates with different HTA parameters

Sample	Off-axis XRD ω -scan FWHM (arcsec)		W–H plot	
	(10-10)	(20-20)	<i>c</i> -Axis LCL (nm)	BSF density ($\times 10^4$ cm ⁻¹)
<i>a</i> -AlN templates annealed at different temperatures for 60 min				
1500 °C	1933	1054	368	2.71
1600 °C	1227	835	416	2.40
1650 °C	1076	954	1130	0.88
1700 °C	1022	964	1333	0.74
1750 °C	1202	964	675	1.48
<i>a</i> -AlN templates annealed at 1700 °C for different time				
60 min	1022	964	1333	0.74
120 min	1008	903	1549	0.64
180 min	1011	910	1797	0.55
240 min	982	864	1524	0.65
480 min	964	838	1431	0.69

summarized in Table 1. From Table 1, we can observe that the *c*-axis LCLs estimated by the modified W–H model increase as the annealing temperature rises from 1500 °C (~368 nm) to 1700 °C (~1333 nm). This result indicates that the crystal grains coalesced during the HTA process and thus the density of the crystal grains decreased. This demonstrates that the density of the defects decreased. Moreover, as shown in Table 1, the estimated BSFD of *a*-AlN layers was reduced by about an order of magnitude as the annealing temperature rises from 1500 °C to 1700 °C, whereas the BSFD increases with the annealing temperature further rising to 1750 °C. The results indicate that the *a*-AlN sample annealed at 1700 °C has the best crystal quality. Based on the above analysis, the BSFDs and LCLs of the *a*-AlN templates annealed at 1700 °C with different annealing time are also calculated and shown in Table 1. As can be seen from Table 1, the sample annealed at 1700 °C for 180 min has the largest grain size and the smallest BSFD (~5500 cm⁻¹). This minimum BSFD is quite remarkable compared to that currently reported for *m*-plane AlN and *a*-plane GaN (BSFD ~ 5000 cm⁻¹).^{11,26} The representative works on nonpolar AlN fabricated on the sapphire substrates are listed in Table 2, in which the FWHMs and BSFDs are used to reflect the crystal quality of the nonpolar AlN samples.

In *a*-plane III-nitride materials, it has been reported that the BSFs, bounded by Frank–Shockley PDs, are the main contributors to the defect density because the formation of the BSFs and PDs is more energetically favorable than that of the perfect dislocations. Thus, the behavior of BSFs can be reflected by the cross-sectional TEM results of both BSFs and PDs. The cross-sectional TEM along the [1-100] axis of the *a*-AlN samples without/with 1700 °C annealing was taken as $\mathbf{g} = 11-20$ to analyze the behavior of the SFs. The invisible criterion of the BSFs and PSFs is $\mathbf{g} \times \mathbf{R} = 0$ or an integer, where the \mathbf{R} represents the displacement vector. The BSFs are bounded with the PDs, and the invisible criterion of the PDs is $\mathbf{g} \times \mathbf{b} < 1/3$, where \mathbf{b} represents the Burgers vectors of dislocations. The PSFs ($\mathbf{R} = \pm 1/2\langle 101-1 \rangle$), BSFs and PDs (\mathbf{R} or $\mathbf{b} = \pm 1/6\langle 20-23 \rangle$ or $\pm 1/3\langle 10-10 \rangle$) can be observed when adopting $\mathbf{g} = 11-20$. The BSFs bounded by PDs are aligned with relatively long lengths along the [1-100] direction and the PSFs should show a band contrast according to the relationship between the stacking fault arrangement and crystal orientation.²⁷ The invisible criteria for perfect dislocations ($\mathbf{b} = \pm\langle 0001 \rangle$ for edge dislocation and $\mathbf{b} = \pm 1/3\langle 11-20 \rangle$ for screw dislocation in *a*-plane III-nitrides) is $\mathbf{g} \times \mathbf{b} = 0$. Thus, the edge dislocation is invisible and the dislocation with screw components is visible when adopting $\mathbf{g} = 11-20$. However, based on the former work from ref. 27, the density of the perfect dislocation is much lower than that of the BSFs (PDs), because the formation of BSFs bound by PDs is energetically favorable compared to perfect dislocations. As a result, the lines in the cross-sectional TEN image are mainly contributed by BSFs and PSFs. The cross-sectional TEM image of the *a*-AlN without annealing is exhibited in Fig. 2(a), and there is a high density of vertical



Table 2 Representative works on nonpolar AlN fabricated on sapphire substrates

Samples (method)	Thickness	FWHM (arcsec)	BSFDs (cm ⁻¹)	Ref.
<i>a</i> -AlN (HVPE: NH ₃ preflow)	1 μm	(11-20) _{//} [1-100]: 1210 (11-20) _{//} [0001]: 1260	—	16
<i>a</i> -AlN (MOCVD and HVPE: NH ₃ preflow and annealing)	10 μm	(11-20) _{//} [1-100]: 660 (11-20) _{//} [0001]: 700	—	9
<i>a</i> -AlN (MOCVD: two-step growth)	2 μm	(11-20) _{//} [1-100]: 1430 (11-20) _{//} [0001]: 2100	—	17
<i>m</i> -AlN (magnetron sputtering and HTA)	275 nm	(10-10) _{//} [11-20]: 684 (10-10) _{//} [0001]: 864	5.0 × 10 ³	11
<i>m</i> -AlN (MOCVD and HTA)	550 nm	(10-10) _{//} [11-20]: 800 (10-10) _{//} [0001]: 1030	1.5 × 10 ⁴	7
<i>a</i> -AlN (magnetron sputtering and HTA)	200 nm	(11-20) _{//} [1-100]: 914 (11-20) _{//} [0001]: 910	5.5 × 10 ³	This work

defects propagating through the *a*-AlN film and the density is too high to distinguish each BSF or dislocation. The defects mainly propagate along the growth direction. After annealing at 1700 °C, the density of the defects decreased significantly as shown in Fig. 2(b). The defects in the blue rectangle are the PSFs because of the band contrast. However, the projection length of PSFs on the section surface is not a certain value, which makes it hard to analyze the behavior of PSFs during HTA. Based on the fact that the BSFs should propagate to the sample surface or annihilate with each other, the defects in Fig. 2(b) can be further determined except for the fragmentary area.^{28,29} The defects in the yellow and red rectangle are the BSFs (or PDs), and the interrupted defect lines without the mark are perfect dislocations. Because the perfect dislocation can bend to the outside of the section, which makes it seem interrupted in the TEM images. The defects in the red rectangle are considered to be the BSFs (or PDs) because of the relatively long lengths. It can be clearly observed that the two BSFs in the red rectangle gradually bend and annihilate each other. The defects lines (two pairs of BSFs) in the yellow rectangle also indicate that the defects (PSFs or BSFs) will annihilate with each other during high-temperature annealing. It can be found that the two outside BSFs and the two inside BSFs annihilate each other, respectively. The reason for this phenomenon is extrapolated that the lattice sequence between one pair of BSFs is different from the overall crystal, and the HTA process can provide enough driven energy to rearrange the lattice sequence and thus annihilate the BSFs. As results, the

annihilation mode for one pair of BSFs is shown in the red rectangle, and the annihilation mode for the two pairs of BSFs is shown in the yellow rectangle.

In order to explain the mechanism of the reduction of BSFs during HTA process, the transition energy barriers are investigated during the elimination of the I₁-type BSF, which is the majority of BSFs (proportion >90%) in *a*-AlN.^{30,31} The wz-AlN supercell is built as shown in structure A of Fig. 3, and the stacking sequence of atoms is [...AaBbAaBb...] along the [0001] direction (capital letters correspond to Al, lowercase letter correspond to N). The I₁-type BSF is built with the stacking sequence of [...AaBbCcBbCcBbAaBb...] along the [0001] direction (denoted as 2-layer-I₁-AlN, as shown in structure I of Fig. 3). The minimum energy pathway from the 2-layer-I₁-AlN to wz-AlN was calculated by the climbing-image nudged elastic band (CI-NEB) method. The energy barriers and the atomic structures during the reaction are shown in Fig. 3. The computational details are shown in the ESI.[†]²³ The atoms that tend to move to the new equilibrium positions are circled in yellow dashed rectangles, and the positions of the BSFs' boundaries (the PDs) are marked by translucent black lines, approximately.

The calculated results indicate that the total energy of 2-layer-I₁-AlN is about 0.39 eV higher than that of the perfect wz-AlN. During the elimination of the stacking fault (from structures I to A), there are four local energy barriers (structure B, D, F, H) that are about 5.10–5.49 eV higher than the initial state of wz-AlN, two metastable states (structure C, G) that are about 1.85 eV higher than wz-AlN, and a local stable state (structure E) that is 0.31 eV higher than wz-AlN. Structure E has the same stacking sequence with the I₃-type BSF of AlN [...AaBbCcBbAaBb...]. It can be inferred that the I₃-type BSF is the intermediate state during the elimination of the I₁-type BSF. The highest energy barrier to eliminate the I₁-type stacking default is 5.032 eV (from the structure I to H) and the highest energy barrier to form the I₁-type stacking fault is 5.204 eV (from structure A to I). It means that when the driven energy (mainly obtained from the annealing temperature) is higher than 5.032 eV and lower than 5.204 eV, the annihilation of I₁-type stacking faults is the main reaction. As exhibited in Fig. 3, when the BSFs are observed

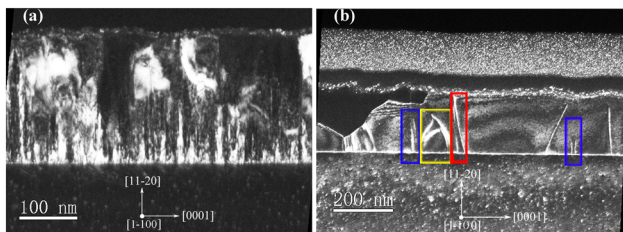


Fig. 2 Cross-sectional TEM images of *a*-AlN templates (a) without annealing and (b) annealed at 1700 °C for 60 min, which are taken near the [1-100] axis with $g = 11-20$.



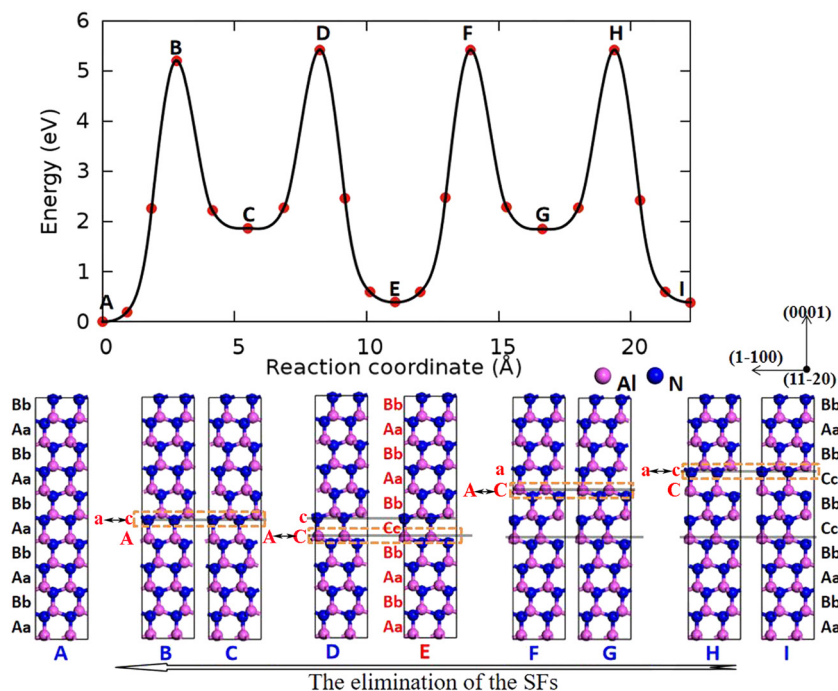


Fig. 3 Top: The minimum energy pathway during the reaction from w-z-AlN (A) to 2-layer-I₁-AlN (I). Bottom: The corresponding structures of the energy barriers and local metastable states. The locations of the SFs are marked by grey lines and the orange-coloured rectangles are used to mark the representative atoms with obvious displacement.

from (11-20) and (1-100) directions, the two BSFs will bend and move closer to each other during HTA, which is consistent with the TEM results as shown in Fig. 2(b). Driven by high temperature, the atoms of structure I tend to vibrate and finally move to the locations, which will provide minimum system energy. During the process, some energy barriers will be overcome to reach the minimum energy. The locations of the SFs are marked by grey lines and the orange-coloured rectangles are used to mark the representative atoms with obvious displacement. From the structure I to structure E, as shown in Fig. 3, the atoms at Cc positions near the orange-coloured rectangles move to the Aa positions, which makes the two I₁-type stacking faults move closer to each other and even turn into I₃-type stacking faults with the lattice sequence of [...AaBbCcBbAa...]. The related phenomenon is shown in the red rectangle in Fig. 2 that the top of two stacking faults is closer than the bottom of the two stacking faults. From structure E to structure A, the atoms at Cc positions of the I₃-type stacking fault [...AaBbCcBbAa...] will also move to Aa positions [...AaBbAaBbAa...] and thus annihilate the stacking faults. However, when the annealing temperature is higher than a certain threshold temperature and the driven energy is higher than the highest energy barrier from structure A to structure I (5.204 eV), the I₁-type stacking faults will be formed, which is a contrary process to the process of stacking fault annihilation. As a result, with the increasing annealing temperature, the BSFD should show decreasing tendency at first and then convert to an increasing tendency, which is in

agreement with the variation tendency of the XRC results as shown in Table 1 and Fig. 1.

The stress state of the AlN epilayers should be changed when the recrystallization process occurs in *a*-AlN templates because the annihilation of BSFs attenuates the BSF's function of releasing the stress induced by the mismatch between AlN and sapphire substrate.^{32,33} To verify the above conclusion, the Raman spectra of *a*-AlN under different annealing conditions were taken and shown in Fig. 4. The dotted lines in Fig. 4 (670.8 and 657.4 cm⁻¹) are the phonon frequencies of E₁(TO) and E₂(high) for strain-free AlN, respectively.³⁴⁻³⁶ Here, we extracted the E₁(TO) and E₂(high) peak positions of all the *a*-AlN samples from the Raman curves in Fig. 4(a) and (c), and the results are summarized in Fig. 4(b) and (d) respectively. From Fig. 4(b) and (d), it can be observed that the position of the E₂(high) peak for the *a*-AlN template without annealing is lower than 657.4 cm⁻¹, which indicates that the as-sputtered *a*-AlN film is under tensile stress. The Raman peaks of *a*-AlN templates blue shifted after the HTA process, which meant the increase of compressive stress in the *a*-AlN layer. Combining the results of Fig. 4(b) and (d) with the results of Fig. 1 and Table 1, it can be found that the blue-shift of the Raman peaks increases with the decreasing BSFD, which means that the compressive stress was accumulated with the decrease in BSFD.³⁷ Hence, the maximum compressive strain was generated in the *a*-AlN sample annealed at 1700 °C for 180 min. Correspondingly, according to XRC results, the *a*-AlN template annealed at 1700 °C for 180 min has the largest grain size and lowest



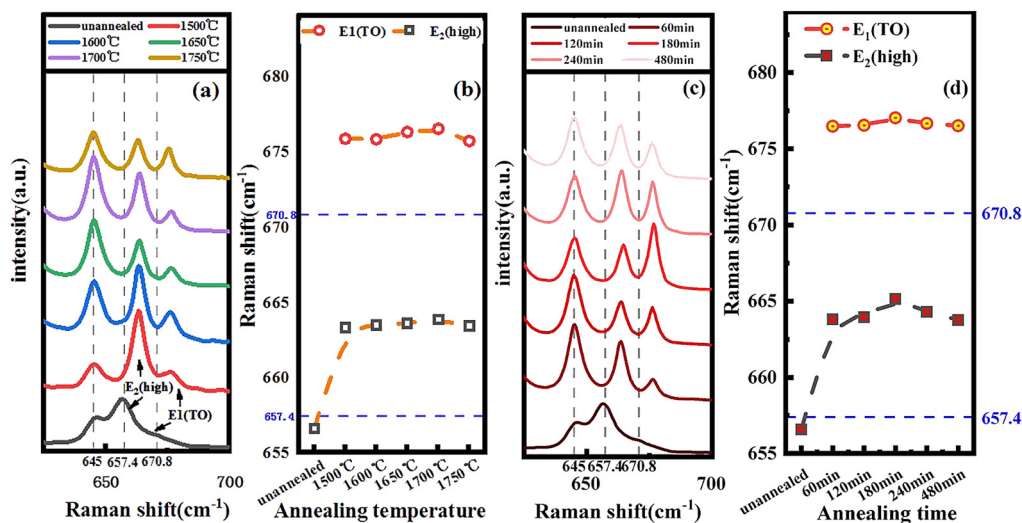


Fig. 4 (a) Room Raman spectra and (b) the positions of the $E_1(\text{TO})$ and $E_2(\text{high})$ peaks of $a\text{-AlN}$ annealed at different temperatures for 60 min. (c) Room Raman spectra and (d) the positions of the $E_1(\text{TO})$ and $E_2(\text{high})$ peaks of $a\text{-AlN}$ annealed at 1700 °C with different annealing times.

BSFD, which is well consistent with the results of the Raman spectra.³⁸

Conclusions

In summary, the annihilation mechanism of BSFs during the HTA process was investigated in the present work. The XRC measurement and the modified Williamson–Hall model calculation results demonstrated that the optimal $a\text{-AlN}$ with a minimal BSFD of $\sim 5500\text{ cm}^{-1}$ was obtained at an annealing temperature of 1700 °C for 180 min. Additionally, the calculated LCL and the cross-sectional TEM results proved that the recrystallization took place during the HTA process. To uncover the annihilation mechanism of BSFs, the minimum energy pathway of the I_1 -type BSF elimination process was investigated by first-principle calculations. The results showed that two I_1 -type stacking faults transformed into one I_3 -type stacking fault as the intermediate state and then were annihilated. Furthermore, the first-principle calculation and Raman spectra results also well explained the BSFD variation tendency that decreases at first and then increases with the rise in the annealing temperature. The work provides further comprehension of the improvement mechanism of $a\text{-AlN}$ by the HTA method, which is vital for the fabrication of high-quality $a\text{-AlN}$ and related devices.

Author contributions

Xiaojuan Sun contributed to data curation, formal analysis, and writing review and editing; Jiaen Sui, JianWei Ben, and Hang Zang contributed to methodology and writing – original draft; Ke Jiang and Shunpeng Lv contributed to the investigation; Shanli Zhang contributed to the project administration; Zhiming Shi and Tong Wu contributed to the resources; Dabing Li contributed to conceptualization and funding acquisition.

Conflicts of interest

There are no conflicts to declare.

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