Switchable Truncations Between the 1st- and 2nd-Order DZT-CFS-UPMLs for Relevant FDTD Problems

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Abstract—Adopting the direct Z-transform (DZT) method due to its higher accuracy instead of the approximate Z-transform (AZT) methods and efficient and switchable truncations between the 1st- and 2nd-order uniaxial perfectly matched layers (UPMLs) with the complex-frequency-shifted (CFS) scheme are shown to terminate the relevant finite-difference time-domain $(FDTD) \ \ regions. \ \ The \ \ proposed \ \ DZT\text{-}CFS\text{-}UPML \ \ formulations$ can possess the switchable function in terms of relevant FDTD problems so that the optimal performance can be obtained with the tradeoff among memory requirement, CPU time, and absorption accuracy. For the FDTD problem with the strong evanescent and weak low-frequency propagating waves, the proposed DZT-CFS-UPML formulations can be switched to the 1st-order PML truncation, and for the other cases with both low-frequency propagating and strong evanescent waves, the 2ndorder PML is the best choice. Two numerical simulations have been carried out to illustrate the validity and flexibility of the proposed approach.

Index Terms—Complex-frequency-shifted uniaxial perfectly matched layer (CFS-UPML), direct Z-transform (DZT) method, finite-difference time-domain (FDTD), switchable function.

I. Introduction

BY USING unsplitted-field implementations, the stretched coordinate perfectly matched layer (SC-PML) [1]–[9] and the uniaxial PML (UPML) [10], [11] have been developed to consume less CPU time and memory to great extent,

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since the splitted-field-based PML method was first proposed in 1994 [12] to terminate the regular finite-difference time-domain (FDTD) computational region [13]. Generally, PML expressions are usually defined and written in the frequency domain. So far, several techniques have been successfully utilized to discretize PML formulations by adopting the auxiliary differential equations (ADEs) techniques [1], [2] or the Z-transform methods [3]–[8]. Why are Z-transform methods quite popular and prevailing for the discretization in FDTD implementations? The main reason is that the convolution in the time domain is just a kind of multiplication in the Z-domain; however, complicated convolutional computations will be never circumvented if the transformation happens from the frequency domain to the time domain [14], [15].

In addition, as described in [14] and [15], two classes of the *Z*-transform techniques can be chosen. The first one is the direct *Z*-transform (D*Z*T) method, which is the most accurate due to the fact that it can convert from terms in the frequency domain to those in the *Z* domain via looking them up in a table; and the another one is the matched *Z*-transform (M*Z*T) and bilinear *Z*-transform (B*Z*T) methods that are always easier due to using direct substitution.

To the best of our knowledge, however, the regular SC and UPMLs have the same drawback as the regular PML, leading to their low efficiencies in absorbing evanescent waves. To conquer this problem, authors proposed the complex-frequency-shifted PML (CFS-PML) formulations, resulting in highly effective absorption for strong evanescent waves and reducing the late-time reflections [16]–[21].

Recently, to pursuing higher accuracies, several higher order PML implementations have been presented for truncating the FDTD domain [22]–[27]. Besides, among these higher order PMLs, the 2nd-order PML has been validated and proved to be an optimal choice [28].

As is well known to all, for the problem with the strong evanescent and weak low-frequency propagating waves, the 1st-order PML is the optimal choice, so that more CPU time and memory requirement can be saved; and for the other cases with both the low-frequency propagating and strong evanescent waves, the 2nd-order PML is the best choice for higher accuracies, although more CPU time and memory are required.

To achieve both higher accuracy in absorption performance and lower consumption in CPU time and memory,

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the DZT-based FDTD implementation adopting SC-PML formulations with the CFS scheme is shown in [29]. Depending on this successful work in [29], therefore, switchable truncations between the 1st- and 2nd-order DZT-based CFS-UPMLs are studied in this work to enrich choices of DZT-based UPML implementations and make themselves easily mastered and used by beginners. In this paper, efficient FDTD implementations of 1st- and 2nd-order DZT-based CFS-UPMLs are proposed to truncate relevant FDTD cases, and this method is here referred as the DZT-CFS-UPML.

This paper is properly organized as follows. In Section II, the proposed DZT-based CFS-UPMLs are developed. Two numerical examples are presented in Section III. Section IV concludes this paper.

II. FORMULATIONS

In 3-D UPML regions, the modified Maxwell's curl equations in the frequency domain can be described as follows:

$$j\omega\varepsilon_0\varepsilon_r(\omega)\Lambda(\omega)E(\omega) = \nabla \times H(\omega) \tag{1}$$

$$j\omega\mu_0\mu_r(\omega)\Lambda(\omega)H(\omega) = -\nabla \times E(\omega) \tag{2}$$

where both ε_r and μ_r are the relative permittivity and permeability in the FDTD domain, respectively, and $\Lambda(\omega)$ is a diagonal tensor defined as follows:

$$\Lambda(\omega) = \operatorname{diag}\left\{\frac{S_{y}S_{z}}{S_{x}}, \frac{S_{x}S_{z}}{S_{y}}, \frac{S_{x}S_{y}}{S_{z}}\right\}$$
(3)

where S_{η} , $(\eta = x, y, z)$ are complex stretched coordinate variables defined as follows:

$$S_{\eta} = \prod_{i=1}^{2} S_{i\eta} = \prod_{i=1}^{2} \left(\kappa_{i\eta} + \frac{\sigma_{i\eta}}{\alpha_{i\eta} + j\omega\varepsilon_{0}} \right) \tag{4}$$

where $\kappa_{i\eta}$ is real and ≥ 1 , and $\sigma_{i\eta}$ and $\alpha_{i\eta}$ are assumed to be the positive real. It should be noted that we here adopt the one- and two-pole CFS-UPMLs. To let the CFS-UPML be absolutely independent of the material attributes of the FDTD computational domains, both (1) and (2) can be rewritten in terms of the electric flux density D and the magnetic flux density B, respectively, [23], [24]

$$j\omega\Lambda(\omega)D(\omega) = \nabla \times H(\omega) \tag{5}$$

$$i\omega\Lambda(\omega)B(\omega) = -\nabla \times E(\omega) \tag{6}$$

Therefore, this kind of UPML can be used for truncating any media, such as dispersive, lossy, inhomogeneous, anisotropic, or nonlinear with no any changes. This method can be obtained in [27] to get H from B [and E from D].

To simplify the left-hand side of expressions in (5) and (6), two auxiliary variables F and G in the frequency domain can be used to denote the right-hand side of (5) and (6), we have

$$F(\omega) = j\omega\Lambda(\omega)D(\omega) \tag{7}$$

$$G(\omega) = j\omega\Lambda(\omega)B(\omega) \tag{8}$$

Now, let us take the discretization of the x component of (7) in the corner of UPML regions, which can be obtained as follows:

$$F_{x}(\omega) = j\omega \Lambda_{x}(\omega) D_{x}(\omega). \tag{9}$$

Rearranging (9), we obtain

$$D_x(\omega) = j\omega^{-1} \left(\frac{S_y S_z}{S_x}\right)^{-1} F_x(\omega). \tag{10}$$

Here, the 1st-order CFS-UPML is considered in (10).

Multiplying $(j\omega^{-1}/j\omega^{-1})$ in the right-hand side of (10), we have

$$D_{x}(\omega) = \left(\frac{j\omega S_{y} \cdot j\omega S_{z}}{j\omega S_{x}}\right)^{-1} F_{x}(\omega). \tag{11}$$

Let us assume $J_{\eta}(\omega) = j\omega S_{\eta}(\omega), (\eta = x, y, \text{orz})$, we have

$$J_{\eta} = \frac{j\omega(\kappa_{\eta}\alpha_{\eta} + \sigma_{\eta}) + (j\omega)^{2}\kappa_{\eta}\varepsilon_{0}}{j\omega\varepsilon_{0} + \alpha_{\eta}} = \frac{j\omega\kappa_{\eta}(j\omega + A_{1\eta})}{j\omega + A_{2\eta}}$$
(12)

Tidying up (12), and we have

$$J_{\eta}^{-1} = \frac{A_{3\eta}}{j\omega + A_{1\eta}} + \frac{A_{4\eta}}{j\omega}$$
 (13)

where

$$A_{1\eta} = \frac{\alpha_{\eta}}{\varepsilon_{0}} + \frac{\sigma_{\eta}}{\kappa_{\eta}\varepsilon_{0}}, \quad A_{2\eta} = \frac{\alpha_{\eta}}{\varepsilon_{0}},$$

$$A_{3\eta} = \frac{1}{\kappa_{\eta}} \left(1 - \frac{A_{2\eta}}{A_{1\eta}} \right), \quad A_{4\eta} = \frac{A_{2\eta}}{\kappa_{\eta}A_{1\eta}}.$$

Rearranging (13) with $\varphi_{\eta} = J_{\eta}^{-1}, (\eta = x, y, \text{ or } z)$ below

$$D_x(\omega) = \frac{\varphi_y \varphi_z}{\varphi_x} F_x(\omega). \tag{14}$$

Next, introducing two auxiliary variables, ϕ_x , δ_x , we achieve

$$D_x(\omega) = \varphi_Z(\omega)\phi_X(\omega) \tag{15}$$

$$\phi_{x}(\omega) = \varphi_{y}(\omega)\delta_{x}(\omega) \tag{16}$$

$$\delta_{x}(\omega) = (1/\varphi_{x}(\omega))F_{x}(\omega). \tag{17}$$

And then, we here adopt the DZT method and reach new DZT-based equations, which can be discretized as follows:

$$P_x^{n+1} = \frac{(A_{3x} + A_{4x}e^{-A_{1x}\Delta t})}{(A_{3x} + A_{4x})}P_x^n + F_x^{n+1} - F_x^n$$
 (18)

$$\delta_x^{n+1} = P_x^{n+1} - e^{-A_{1x}\Delta t} P_x^n \tag{19}$$

$$\hat{\delta}_x^{n+1} = \hat{\delta}_x^n + A_{4y} \Delta t \delta_x^{n+1} \tag{20}$$

$$\phi_x^{n+1} = e^{-A_{1y}\Delta t}\phi_x^n + \hat{\delta}_x^{n+1} - e^{-A_{1y}\Delta t}\hat{\delta}_x^n$$

$$+A_{3y}\Delta t\delta_x^{n+1}$$
 (21)

$$\hat{D}_x^{n+1} = \hat{D}_x^n + A_{4z} \Delta t \phi_x^{n+1} \tag{22}$$

$$D_x^{n+1} = e^{-A_{1z}\Delta t} D_x^n + \hat{D}_x^{n+1} - e^{-A_{1z}\Delta t} \hat{D}_x^n$$

$$+A_{3z}\Delta t\phi_x^{n+1} \tag{23}$$

where P_x , $\hat{\delta}_x$, \hat{D}_x are introduced as auxiliary variables in (18)–(23).

The simulation pseudo-code of (18)–(23) is as follows: 1st step:

temp_
$$Fx = F_x^n$$
, temp_ $\delta x = \delta_x^n$
temp_ $Px = P_x^n$, temp_ $D_x^n = D_x^n$
temp_ $\phi x = \phi_x^n$, temp_ $\hat{D}_x^n = \hat{D}_x^n$, temp_ $\hat{\delta}_x^n = \hat{\delta}_x^n$.



Fig. 1. FDTD grid geometry in this simulation.

2nd step:

$$P_x^{n+1} = \frac{(A_{3x} + A_{4x}e^{-A_{1x}\Delta t})}{(A_{3x} + A_{4x})} \text{temp_}Px + F_x^{n+1} - \text{temp_}Fx.$$

3rd step:

$$\delta_x^{n+1} = P_x^{n+1} - e^{-A_{1x}\Delta t} \text{temp } Px$$

4th step:

$$\hat{\delta}_{r}^{n+1} = \text{temp } \hat{\delta}_{r}^{n} + A_{4y} \Delta t \delta_{r}^{n+1}$$

5th step:

$$\begin{aligned} \phi_x^{n+1} &= e^{-A_{1y}\Delta t} \text{temp}_{-}\phi x + \hat{\delta}_x^{n+1} - e^{-A_{1y}\Delta t} \text{temp}_{-}\hat{\delta}_x^{n} + A_{3y}\Delta t \delta_x^{n+1}. \end{aligned}$$

6th step:

$$\hat{D}_x^{n+1} = \text{temp}_{\perp} \hat{D}_x^n + A_{4z} \Delta t \phi_x^{n+1}.$$

7th step:

$$D_x^{n+1} = e^{-A_{1z}\Delta t} \text{temp } D_x^n + \hat{D}_x^{n+1} - e^{-A_{1z}\Delta t} \text{temp } \hat{D}_x^n + A_{3z}\Delta t \phi_x^{n+1}$$

Similar operations can be applied to 2nd-order DZT-CFS-UPML.

III. NUMERICAL RESULTS

To reflect preferable performances between the proposed 1st- and 2nd-order DZT-CFS-UPML approaches for relevant FDTD cases so that we can judge which one is the best choice for the corresponding FDTD case, we get ready to adopt commonly used 2-D and 3-D cases for assessing their comprehensive performances.

In the first case, a 2-D TE-polarized electromagnetic wave interaction with an infinitely long perfectly electric conductor (PEC) sheet with the finite width is applied to illustrating the validity of the proposed DZT-CFS-UPMLs.

The space is discretized with $\Delta x = \Delta y = 1$ mm and time step is $\Delta t = 1.1785$ ps. The FDTD computational domain consists of a 100-cell wide PEC sheet surrounded by free space. The ten cell-thick PML layers are used to terminate the grid and are placed only three cells away from the PEC sheet in all directions, shown in Fig. 1.

A y-polarized line electric current source, infinitely long in the z-direction, is placed at the center position and excited with the differentiated Gaussian pulse [26]. The y-component of the electric field is measured at the observing point P, where we expect very strong evanescent waves to appear.

The relative reflection error (in dB) versus time steps is computed at the observation point P. The reference grid is

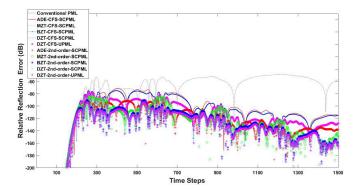


Fig. 2. Relative reflection error versus time steps.

TABLE I
PERFORMANCES FOR DIFFERENT PML IMPLEMENTATIONS

PML algorithms	MRRE	Memory	CPU time
	(dB)	(bytes)	(s)
Conventional PML	-49.1982	1,324 K	66.79
ADE-CFS-SCPML	-71.4797	1,161 K	66.51
MZT-CFS-SCPML	-73.6765	1,176 K	66.75
BZT-CFS-SCPML	-74.9075	1,172 K	67.25
DZT-CFS-SCPML	-77.2969	1,281 K	74.95
DZT-CFS-UPML	-77.7969	1,403 K	80.65
ADE-2 nd -order-SCPML	-90.4784	1,375 K	88.95
MZT-2 nd -order-SCPML	-84.3734	1,353 K	88,65
BZT-2 nd -order-SCPML	-90.2828	1,353 K	88.95
DZT-2 nd -order-SCPML	-93.7828	1,457 K	88.95
DZT-2 nd -order-UPML	-93.7828	1,711 K	89.95

sufficiently large such that there are no reflections from its outer boundaries during 1500 time steps, which are well past the steady-state response.

The details of PML parameters have been presented to obtain the lowest reflection, shown as follows.

- 1) For the conventional PML, $\kappa_{\text{max}} = 9$ and $\sigma_{\text{max}} = 0.6\sigma_{\text{opt}}$ are chosen
- 2) For the CFS-PML, $\kappa_{\rm max} = 9$, $\sigma_{\rm max} = 0.9 \sigma_{\rm opt}$, and $\alpha_{\eta} = 0.05$ are chosen.
- 3) For the 2nd-order PML, the following parameters are chosen:

$$\kappa_{1\eta} = 1, \alpha_{1\eta} = 0, \sigma_{1\eta\text{opt}} = 0.075/150\pi \,\Delta x, \sigma_{1\eta} = \sigma_{1\eta\text{opt}}\rho^4$$

$$\sigma_{2\eta\text{opt}} = 4/150\pi \,\Delta x, \sigma_{2\eta} = \sigma_{2\eta\text{opt}}\rho^2, \kappa_{2\eta} = 1 + \kappa_{2\eta\text{opt}}\rho^2,$$

$$\kappa_{2\eta\text{opt}} = 10, \text{ and } \alpha_{2\eta} = 0.08 + \sigma_{1\eta}.$$

These optimum parameters are empirically chosen to reach the lowest reflection.

The results are illustrated in Fig. 2. The maximum relative reflection errors (MRRE), memory requirements, and CPU time consumption (time steps $=20\,000$) for these PMLs are shown in Table I.

As it is reflected in Fig. 2 and Table I that the case has been used to validate all FDTD methods with PML scheme. In Fig. 2, the proposed 1st-order DZT-CFS-UPML has similar accuracy with the 1st-order DZT-CFS-SCPML.

However, for this 2-D case, we can see in Fig. 2 that the 2nd-order one has more obvious improvement than the

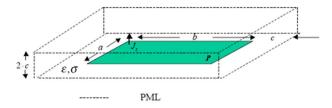


Fig. 3. FDTD grid geometry in this simulation.

1st-order one, although a bit more time and memory are required, shown in Table I. Therefore, the 2nd-order DZT-CFS-UPML can be considered as the preferable choice when solving 2-D FDTD problems.

It should be noted in the first case, however, that the advantages of the 1st-order DZT-CFS-UPML is not quite obvious due to only solving the 2-D case. To better reflect its advantages, therefore, the 3-D problem of the electromagnetic scattering by a highly elongated object is studied [29].

The thin plate with the 100 mm \times 25 mm size is immersed in a background media [29] with constitutive parameters σ and ε , shown in Fig. 3. For the purpose of this study, the constitutive parameters for soil are assumed, using $\varepsilon_r = 7.73$ and $\sigma = 0.273$. The numerical test is implemented and composed of a $126 \times 51 \times 26$ grid, which includes ten cell-thick PML. The space is discretized with the FDTD lattice with $\Delta x = \Delta y = \Delta z = 1$ mm and the time step is $\Delta t = 5.3$ ps. In total, 2000 time steps are used for computing the relative reflection error versus time at an observation point. All similar details of this numerical simulation can be found in [29].

The details of PML parameters have been presented to obtain the lowest reflection, shown as follows.

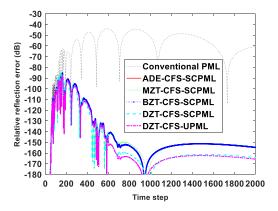
- 1) For the conventional PML, $\kappa_{\rm max}=14$ and $\sigma_{\rm max}=0.56\sigma_{\rm opt}$ are chosen.
- 2) For the CFS-PML, $\kappa_{\text{max}} = 11$, $\sigma_{\text{max}} = 0.4\sigma_{\text{opt}}$, and $\alpha_{\eta} = 0.05$ are chosen.
- 3) For the 2nd-order PML, the following parameters are chosen:

$$\kappa_{1\eta} = 1, \alpha_{1\eta} = 0, \sigma_{1\eta\text{opt}} = 0.075/150\pi \,\Delta x, \sigma_{1\eta} = \sigma_{1\eta\text{opt}}\rho^4,
\sigma_{2\eta} = \sigma_{2\eta\text{opt}}\rho^2, \kappa_{2\eta} = 1 + \kappa_{2\eta\text{opt}}\rho^2, \kappa_{2\eta\text{opt}} = 14,
\alpha_{2\eta} = 0.06 + \sigma_{1\eta}, \text{ and } \sigma_{2\eta\text{opt}} = 4/150\pi \,\Delta x.$$

These optimum parameters are empirically chosen to reach the lowest reflection.

As seen in Fig. 4 and Table II, it can be observed that the 1st- and 2nd DZT-based SC and UPMLs have better absorption with the increasing of time steps and much more reduction in the late-time reflection than the other PMLs based on ADE, BZT, and MZT.

Furthermore, as presented in Table II, the 1st-order DZT-CFS-UPML not only requires much less CPU time and memory than the 2nd-order DZT-CFS-UPML but also obtains very good absorption accuracy, although higher absorption accuracy can be reached using the 2nd-order one. Therefore, the 1st-order DZT-CFS-UPML can be treated as the preferable choice when solving 3-D FDTD problems.



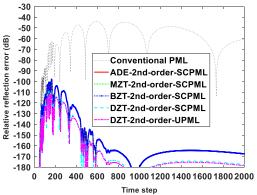


Fig. 4. Relative reflection errors versus time steps for the 1st- and 2nd-order DZT-CFS-UPMLs.

TABLE II
PERFORMANCES FOR DIFFERENT PML IMPLEMENTATIONS

PML algorithms	MRRE	Memory	CPU time
	(dB)	(bytes)	(s)
Conventional PML	-43.9754	26,334 K	780.79
ADE-CFS-SCPML	-85.2538	25,361 K	777.51
MZT-CFS-SCPML	-83.5343	25,276 K	776.75
BZT-CFS-SCPML	-85.2538	25,372 K	777.25
DZT-CFS-SCPML	-85.5343	26,121 K	776.95
DZT-CFS-UPML	-87.2538	28,503 K	798.65
ADE-2 nd -order-SCPML	-97.7774	31,275 K	1031.08
MZT-2 nd -order-SCPML	-97.5969	31,335 K	1033.12
BZT-2 nd -order-SCPML	-97.9582	31,311 K	1031.03
DZT-2 nd -order-SCPML	-107.4053	32,551 K	1061.52
DZT-2 nd -order-UPML	-109.0646	33,221 K	1082.81

IV. CONCLUSION

So far, the validities and stabilities of the proposed 1st- and 2nd-order DZT-CFS-UPMLs have been illustrated. Additionally, for the relevant FDTD cases, we can judge and determine which one is the best choice between 1st- and 2nd-order DZT-CFS-UPMLs, in terms of the tradeoff among CPU time, memory requirement, and absorption accuracy. In a word, due to introducing the DZT techniques, the proposed 1st- and 2nd-order CFS-UPMLs can not only achieve better accuracies than those based on ADE, BZT, and MZT but also provide alternative choices of DZT-based UPML implementations and make themselves easily mastered and used.

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